# Auxiliary material for

1458	S-velocity Model and Inferred Moho Topography beneath the Antarctic Plate
1459	from Rayleigh Waves
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1471	
1472	1. Introduction
1473	This file includes four supplementary sections, and captions of 1 supplementary table
1474	(Table S1) and 7 figures (Figure S1-S7). Table S1 can be found in "01 Seismic
1475	model_ANT_v12_suppl_Table S1_submit.pdf". Figure S1-S7 can be found in
1476	respectively in pdf files of figure_S01.pdf, figure_S02.pdf, figure_S03.pdf,
1477	figure_S04.pdf, figure_S05.pdf, figure_S06.pdf, figure_S07.pdf.

1479	2. The Antarctic Plate and its Tectonic History
1480	The Antarctic Plate consists of the Antarctic continent and the surrounding oceanic
1481	regions. The continent comprises three primary tectonic regions: East Antarctica
1482	(EANT), West Antarctica (WANT), and the Transantarctic Mountains. EANT is stable,
1483	topographically high, and is thought to feature Precambrian continental lithosphere
1484	[Bentley, 1991]. In contrast, WANT is an amalgamation of low-lying, younger crustal
1485	micro-blocks [Dalziel and Elliot, 1982; Talarico and Kleinschmidt, 2008].
1486	
1487	The Antarctic continent was formed from a number of Archean/Early Proterozoic
1488	cratons (older than 1.5 Ga), surrounded by successively younger belts. Amalgamation
1489	occurred through accretionary or collisional events, which were episodically
1490	punctuated by periods of crustal extension and rifting. The younger belts represent the
1491	products of convergent plate tectonic events such as oceanic crust subduction beneath
1492	continental crust and/or continent-continent collision [Talarico and Kleinschmidt,
1493	<u>2008; Boger, 2011]</u> .
1494	
1495	During the Neoproterozoic, the Rodinia supercontinent is postulated to have formed at
1496	~1.0 Ga and broken apart at ~850-800 Ma [Torsvik, 2003]. Within Rodinia, the
1497	Mawson craton of East Antarctica was connected with Western Australia [Fitzsimons,

1498 2003], making up East Gondwana. East Gondwana was connected with Laurentia

1499 (North America). The northern Prince Charles Mountains, the Napier Complex, 1500 Lützow Holm Complex, and Rayner Complex, which are currently part of EANT, were 1501 likely connected with India, making up the Indo-Antarctica continent [Talarico and 1502 Kleinschmidt, 2008; Torsvik, et al., 2008a]. During the break-up of Rodinia, rifting 1503 between East Gondwana and Laurentia began at 750–725 Ma [Dalziel, 1991]. Prior to 1504 550 Ma, West Gondwana, which consisted of Africa and South America, was 1505 connected with the Indo-Antarctica continent. Finally, Gondwana formed when East 1506 Gondwana connected with West Gondwana at ~550 Ma [Boger, et al., 2001; Boger, et 1507 al., 2002; Boger, 2011], see Figure S1a and b. The amalgamation of Gondwana produced the Pan-African orogens, some of the most spectacular mountain-belt 1508 1509 building episodes in Earth's history [Torsvik, et al., 2008a]. However, the 1510 amalgamation suture zone in EANT (the suture zone marked in Figure S1b is 1511 speculated in Boger [2011]) is still not well understood because most of EANT is 1512 covered by ice. At ~250 Ma, Gondwana connected with Laurasia to form the most 1513 recent supercontinent, Pangaea (see Figure S1c).

1514

Pangaea began breaking apart at 180 Ma. The first major tectonic break-up stage corresponded to an initial rifting phase that started in the Weddell Sea in the Late Jurassic [*Lawver, et al.*, 1991]. This rifting led to the separation of Antarctica from South Africa at ~180 Ma, from India at ~130 Ma, and finally from Australia at ~90 Ma [*Veevers*, 1986; *Torsvik, et al.*, 2008a; *Boger*, 2011], see Figure S2. The separation of

1520 Antarctica from South Africa has been attributed to the Bouvet hotspot [*Hawkesworth*, 1521 et al., 1999; Torsvik, et al., 2008a]. The rifting of Antarctica away from India and then 1522 Australia has been attributed to the influence of the Kerguelen hotspot at 140 Ma [Hawkesworth, et al., 1999; Boger, 2011]. By ~110 Ma, the micro-plates of West 1523 1524 Antarctica had nearly reached their present location with respect to East Antarctica 1525 [Talarico and Kleinschmidt, 2008]. At ~83 Ma, Antarctica had reached its final polar 1526 location and the final break-up was completed when New Zealand rifted away from 1527 Marie Byrd Land, WANT [Stock and Molnar, 1987; Lawver, et al., 1991; Larter, et al., 1528 2002; Torsvik, et al., 2008b]. After break-up was complete, geological activity in 1529 Antarctica was limited to on-going extension and volcanism in the West Antarctic Rift 1530 System (WARS). Given Antarctica's shared tectonic history with neighboring 1531 Gondwanan continents (e.g., Africa, India, Australia, Zealandia, and South America), 1532 geological and tectonic similarities naturally exist along and close to the continent 1533 boundaries [Gohl, 2008].

1534

During the tectonic history of Antarctica, all blocks of EANT were amalgamated at ~500 Ma, while WANT, and the whole of Antarctica, were amalgamated at ~110 Ma. For a significant period of Earth's history, Antarctica has held a central position within both the supercontinents of Rodinia (1300–700 Ma) and Gondwana (550–200 Ma) [*Dalziel*, 1991; *Moores*, 1991; *Talarico and Kleinschmidt*, 2008]. The current Antarctic plate was formed primarily during the formation of the Gondwanan supercontinent, 1541 especially during three main periods: (1) c. 600–450 Ma, during the amalgamation of

1542 Gondwana; (2) c. 450–180 Ma, from the end of Gondwanan amalgamation to the onset

1543 of break-up; and (3) c. 180–0 Ma, since the break-up of Gondwana. The geology of the

- 1544 Antarctic continent, particularly the EANT, was established during the first two periods
- 1545 [Talarico and Kleinschmidt, 2008]. During the third period, the oceanic region was
- 1546 formed and WANT was re-formed [*Torsvik, et al.*, 2008a].
- 1547

### 1548 **3. 3D S-velocity model inversion from surface wave dispersion**

For waves with a period of  $P_j$ , the wave propagation path of the *k*-th ray can be discretized and its travel time ( $t_k$ ) expressed as:

$$t_k = G_k \cdot S \tag{1}$$

where  $G_k$  is a row of the observation matrix G with k-th path segment lengths for each discretized cell and S is the surface-wave group/phase slowness (reciprocal of velocity) vector. The relationship between the slowness  $S(P_j)$  of the period  $P_j$  and the perturbation of S-velocity ( $\Delta \beta_i$ ) of the *i*-th layer in a vertical S-velocity model where the wave propagates can be written as:

1557 
$$S(P_j) = S_{\text{Ref}}(P_j) + \sum_{i=1}^n \frac{\partial S}{\partial \beta_i} \Delta \beta_i$$
(2)

where  $S_{\text{Ref}}(P_j)$  is the group/phase slowness of a given reference model and  $\partial S/\partial \beta_i$  is the partial derivative of the group/phase slowness to the *S*-velocity of the *i*-th layer in the reference model. Replacing the vector **S** in Eq. (1) by the slowness in Eq. (2), changes 1561 Eq. (1) to:

$$1562 t_k = \boldsymbol{A}_k \cdot \boldsymbol{B} + \boldsymbol{c}_k (3)$$

where  $A_k$  is a coefficient matrix deduced from operations between matrix  $G_k$  and all partial derivatives  $\partial S/\partial \beta_i$ , **B** is the vector of 3-D S-velocity perturbations to be determined, and  $c_k$  is a constant obtained from the combination of  $G_k$  and  $S_{\text{Ref}}(P_j)$ . For all paths and periods, we can then obtain the travel time vector (**T**) in the following matrix form:

 $1568 T = A \cdot B + C (4)$ 

where  $C (= c_1, ..., c_k, ...)$  is a constant vector. Because Eq. (4) is commonly ill posed, we used the 3D first-order spatial gradient ( $\nabla$ ) of the model as an *a priori* constraint, and the final inversion equation then becomes:

1572 
$$\begin{pmatrix} \boldsymbol{T} - \boldsymbol{C} \\ \boldsymbol{\theta} \end{pmatrix} = \begin{pmatrix} \boldsymbol{A} \\ \lambda \nabla \end{pmatrix} \cdot \boldsymbol{B}$$
(5)

1573 where  $\lambda$  is a weighting factor to balance between fitting of the travel times and model 1574 smoothing. The above equations show that our inversion for S-velocities is a linearized 1575 inversion combining a horizontal 2D surface wave dispersion linear inversion and a 1576 vertical 1D linearized inversion. A detailed description of this method can be found in 1577 <u>Feng and An [2010]</u>.

1578

#### 1579 **4. Spatial resolution analysis**

1580 Resolution lengths of an inverse problem can be retrieved from a resolution matrix that

1581 defines a linear projection [Nolet, 2008; Thurber and Ritsema, 2009; An, 2012]. Our 1582 tomographic inversion for a 3D S-velocity model is, in fact, a linearized inversion, and 1583 a resolution matrix can be outputted at any iteration for a linearized inversion. 1584 However, the matrix cannot give the expected resolution lengths of the final model, but 1585 only an approximate resolution length for a model with respect to a given reference 1586 model. The real model resolution length will depend not only on the reference model, 1587 but also on the nonlinearity of the observation operator in the inverse problem [An, 1588 2012]. Therefore, we do not provide quantitative resolution lengths from the resolution 1589 matrix of the 3D S-velocity inversion. However, we present quantitative resolution 1590 lengths for the horizontal 2D surface wave dispersions, which are useful in evaluating 1591 the lateral resolution of a surface wave study. The lateral resolution lengths were 1592 retrieved by using the statistical resolution length calculation proposed by An [2012]. 1593 Visualization of the inverted solution model from a random synthetic model cannot 1594 only yield resolution length information, but also the direction dependence of the 1595 resolution [An, 2012]. Therefore, in addition to the statistical resolution analyses for 1596 the dispersions, we also analyzed the lateral and vertical resolution from visualization 1597 of the inverted 3D output model using random synthetic 3D input models, based on all 1598 the rays of real observations.

1599

1600 A statistical resolution analysis is simple and independent of the approach and 1601 parameterization used in the inversion. The statistical resolution length calculation

1602 includes two steps. The first step is to create a random synthetic input model, and then 1603 to obtain an output solution using the input model as in a general synthetic test. The 1604 second step is to invert for resolution lengths for all model parameters. A detailed 1605 introduction to these procedures can be found in An [2012]. Figure S3c-e shows the 1606 resolution length distribution for the Rayleigh wave dispersion at periods of 50, 100, 1607 and 150 s. This figure shows that the horizontal resolution length of the whole 1608 continent can be ~100 km for a period of 50 s and ~250 km for a period of 150 s, and 1609 in the oceanic areas are ~200 and ~500 km, respectively.

1610

1611 As described above, it is not possible to obtain a resolution length for the 3D model as 1612 the inversion is nonlinear, and it is also difficult to determine indicative resolution 1613 information by checkerboard tests given the complexity of the model parameterization. 1614 However, a simple method can be used to provide indicative resolution information for 1615 the 3D model. An [2012] noted that even for a random synthetic input model without 1616 specific checkers, an inverse output solution can yield an anomaly pattern similar to 1617 the output of a checkerboard test, which can provide not only resolution length 1618 information but also the direction dependence of the resolution. A synthetic random 1619 model and its solution used in the above statistical resolution analysis to give the 1620 lateral resolution length for a 2D dispersion inversion are shown in Figure S3a and b. 1621 In this figure, even though the inverted solution (Figure S3b) depends on the random 1622 synthetic model (Figure S3a), the solution not only visually provides resolution length 1623 information, but also the direction dependence of the resolution length. In Figure S3b, 1624 most of the anomaly pattern appears as a strip with a long axis along the meridian and 1625 a short axis along the line of the latitude, particularly for the oceanic region where the 1626 anomaly patterns in the input synthetic model (Figure S3a) have little similarity to the 1627 strip anomaly in the solution (Figure S3b). This anomaly pattern indicates that the 1628 resolution length along the meridian is larger than that along the line of latitude. Given 1629 that most of the observation stations are located inside continental Antarctica and that 1630 the earthquakes are coming from the plate boundaries (Figure 1), the rays should 1631 mainly intersect at positions far from the plate boundary and the rays at positions close 1632 to the plate boundary are largely parallel to neighboring rays. In practice, the resolution 1633 length along the parallel direction (i.e., almost parallel to meridian) of the rays should 1634 be greater than in the normal direction (i.e., almost parallel to the line of latitude), 1635 which is consistent with the indicative example of an inverted solution in Figure S3b.

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A visualization of an inverted solution model from a random synthetic model cannot only provide indicative resolution length information, but also the direction dependence of the resolution. As such, we have also indicatively analyzed the lateral and vertical resolution from a visualization of the inverted 3D solution using random synthetic 3D models, based on real ray observations. We created several random synthetic 3D S-velocity models, and obtained the solutions by inverting the synthetic observations from the synthetic models. Figure S4 shows horizontal slices of an 1644 inverted 3D S-velocity solution from one of these random synthetic 3D models. The 1645 solution slices at depths of 50, 120, and 200 km (Figure S4b-d) demonstrate not only 1646 direction dependence of the resolution in the oceanic region, similar to those implied 1647 from Figure S3, but also depth dependence. It should be noted that the inverted 1648 solution of any random model depends on the synthetic model and, therefore, only one 1649 inverted solution from a random synthetic model cannot provide full resolution length 1650 information for the whole area. Given that we only show one solution model here, we 1651 selected a model that indicatively provides resolution length information for a typical region (e.g., GSM). Beneath the region close to the GSM, the checker-like anomaly 1652 1653 extent is at a minimum of ~250 km at depths of 50 km (Figure S4b), ~500 km at depths 1654 of 120 km (Figure S4c), and ~800 km at depths of 200 km (Figure S4d). This indicates 1655 that the horizontal resolution length is ~120 km at a depth of 50 km, ~250 km at a 1656 depth of 120 km, and ~400 km at a depth of 200 km beneath the GSM. In the oceanic 1657 region close to Marie Byrd Land (MBL), the extent of the checker-like anomaly at a 1658 depth of 50 km (Figure S4b) is ~300 km along the short axis and ~1000 km in a direction close to meridian, which indicates that the resolution length at a depth of 50 1659 1660 km is ~150 km along the line of latitude and ~500 km along the meridian. The 1661 checker-like anomaly extent is ~1000 km at a depth of 120 km and ~1500 km at a 1662 depth of 200 km, which indicates that the resolution length is ~500 km at a depth of 1663 120 km and  $\sim$ 750 km at a depth of 200 km.

1665	The two vertical slices shown in Figure S4e and f indicate that the vertical and
1666	horizontal resolution length increases with increasing depth, as expected from
1667	sensitivity of surface wave dispersion with respect to S-velocities (Figure S5). Beneath
1668	the GSM, the vertical extents of the anomalies in this figure are $\sim 20$ km down to 60 km,
1669	~50 km down to 150 km, and ~100 km down to 250 km, which indicates that the
1670	vertical resolution lengths are ~10 km down to 60 km, ~25 km down to 150 km, and
1671	~50 km down to 250 km. The discontinuity in the resolution length should be greater
1672	than that of the velocity model [An, 2012], and the vertical resolution length for the
1673	Moho depth retrieved from the 3D model should be <10 km, because the Moho depth
1674	is mostly <60 km, and for the seismic lithosphere-asthenosphere boundary (LAB)
1675	should be smaller than 25–50 km, because LAB is mostly at the depths of ~100–250
1676	km.

## 1678 5. Antarctic Moho Compilation of AN-Moho

We compiled crustal thicknesses and/or Moho depths (Figure S7a) from active seismic and receiver function studies, and constructed a crustal thickness compilation of ANtarctic Moho positions (AN-Moho; Figure S7c). Even though previous surface wave studies yielded average crustal thicknesses over a large area, we did not compile these crustal thicknesses.

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1685 Using Moho depths beneath scatter points, *Baranov and Morelli* [2013] assembled a

1686 Moho model by kriging interpolation without quality discrimination for Moho depths 1687 published prior to 2012. We have made three improvements over the compilation of 1688 Moho depths by Baranov and Morelli [2013]. First, we included new data collected 1689 after 2012. For example, Moho depths from PRF analyses beneath POLENET stations 1690 in WANT [Chaput, et al., 2014] and from SRF analyses beneath six Chinese EANT 1691 stations [Feng, et al., 2014] at locations where the Moho had not been previously 1692 studied were used here. Second, we evaluated the quality of obtained Moho depths 1693 from the original publications, and discarded poor data with large uncertainties due to 1694 the quality of the observations. For example, we selected Moho depths obtained 1695 beneath TransAntarctic Mountains Seismic Experiment (TAMSEIS) stations over the 1696 ice sheet from Hansen, et al. [2009], but not from Lawrence, et al. [2006], which was 1697 used in Baranov and Morelli [2013]. Third, we corrected all thicknesses using the 1698 same definition of crustal thickness. Therefore, slight differences exist between the 1699 data for AN-Moho as compared with the previous compilation and also the data 1700 presented in the original publications. More details of these screening procedures and 1701 thickness corrections are described below.

1702

The crustal thickness or Moho depth data presented in different publications may use different definitions, which can result in different crustal thickness values beneath the same position. In most RF studies, crustal thickness is defined as the distance from the solid surface to the Moho, and the ice thickness is included in the crustal thickness.

1707 However, Hansen et al. [2009; 2010] and Chaput et al. [2014] defined the crustal 1708 bedrock thickness as representing the crustal thickness, which does not include the ice 1709 thickness. In active-source seismic studies, crustal thickness is often defined as the 1710 distance from sea level to the Moho. We defined crustal thickness as the distance from 1711 the uppermost solid (i.e., ice, sediment, or bedrock) surface to the Moho discontinuity, 1712 and the Moho depth as being from sea level to the Moho discontinuity. If a previous 1713 study presented surface elevation data, we used the given elevation in the conversion 1714 between crustal thickness and Moho depth. Otherwise, the solid surface elevation from 1715 ETOPO2 was used in the conversion. We corrected all the thicknesses or depths in 1716 previous studies in this fashion. After the conversion, different crustal thickness values 1717 may yield the same information. For example, at the station BYRD, the crustal 1718 thickness converted from the result (24.3 km) of Chaput et al. [2014] becomes 26.75 1719 km, which is essentially the same as the value of 27 km of Winberry and 1720 Anandakrishnan [2004].

1721

Crustal thickness can be measured by several types of seismic observations, and even one observation may yield different crustal thicknesses depending on the analytical method applied to the data. Some observations or analytical methods may result in large uncertainties. Therefore, the crustal thicknesses given in previous studies may vary significantly for the same position. Where two or more publications provided crustal thickness data for the same location, we calculated the differences between

1728 these data for each position, and all crustal thicknesses with a difference of >2 km are 1729 shown in Figure S7b. This figure shows that the difference between crustal thicknesses 1730 given by different publications can be as large as ~10 km. In Figure S7b, the 1731 differences are most evident at: (1) between the SRF [Hansen, et al., 2009; Hansen, et 1732 al., 2010] and PRF results [Lawrence, et al., 2006; Finotello, et al., 2011]; and (2) 1733 between the PRF results of Finotello, et al. [2011] and Lawrence, et al. [2006] and 1734 those of the DRV station from Kanao and Shibutani [2012] and Reading [2004]. In 1735 addition to the crustal thicknesses for the stations listed in Figure S7b, crustal thickness 1736 data from only one publication may also have a large uncertainty. Therefore, we 1737 discarded data with large uncertainties that reflect both the observation quality and 1738 analytical method, as outlined below.

1739

1740 PRF analysis has become a general method to rapidly and simply provide a crustal 1741 thickness, and SRF analyses have also been recently used to obtain crustal thickness 1742 data. Generally, the signal-to-noise ratio of the first-arriving P-wave is higher than that of the secondary phase or S-wave, and the wavelength of the PRF is much shorter than 1743 1744 that of the SRF, because the signal frequencies used in a PRF study are typically higher 1745 than those used in a SRF study. Therefore, a Moho depth obtained from a PRF should 1746 have a better resolution than that from a SRF. As such, for land stations where the 1747 difference between the SRF and PRF results was large, we used the PRF results. For 1748 example, we selected data from Lawrence, et al. [2006] rather than Hansen, et al.

1749	[2009] for onland stations (E000–E010 and coastal stations). However, for seismic
1750	stations over the ice cap, the ice is so thick that it influences the PRF more than the
1751	SRF. The PRF analysis of <i>Lawrence, et al.</i> [2006] did not account properly for the ice
1752	sheet and as such the results are poor for stations on the ice sheet [Hansen, et al., 2009]
1753	(i.e., E012-E030 and all N stations). Given this, we selected crustal thickness data
1754	from the SRF analyses of <i>Hansen, et al.</i> [2009], but not from the PRF analyses of
1755	Lawrence, et al. [2006].

An unclear Ps phase in the PRF or Sp phase in the SRF indicates that the Moho discontinuity is not sharp, and the resulting Moho depth from the receiver function may have a large uncertainty. For example, two different Moho depths of 42 km [*Reading*, 2004] and 28 km [*Kanao and Shibutani*, 2012] for the station DRV (Figure S7b) were estimated from inverted S-velocity models by PRF waveforms with an unclear Ps phase.

1763

1764 After an RF waveform is obtained, a Moho depth can be obtained by various methods 1765 [e.g., *Ammon, et al.*, 1990; *Zhu and Kanamori*, 2000; *Chaput, et al.*, 2014]. However, 1766 different methods may result in different calculated Moho depths. For example, the 1767 Moho estimated from a 1D multi-layer S-velocity model inverted from the receiver 1768 function [e.g., *Ammon, et al.*, 1990] may be different with that directly measured by the 1769 H- $\kappa$  stacking method assuming a constant Vp and single crustal layer [*Zhu and* 

1770	<u>Kanamori, 2000</u> ]. The differences between <u>Lawrence, et al. [2006]</u> and <u>Finotello, et al.</u>
1771	[2011], reflect the fact that Lawrence, et al. [2006] used the first method, whereas
1772	Finotello, et al. [2011] used the second method. The differences for some coastal
1773	stations, such as CBOB, also can be interpreted as that which interface was identified
1774	as the Moho differs [ <i>Finotello, et al., 2011</i> ]. For example, <i>Lawrence, et al.</i> [2006]
1775	associated a velocity jump from $\sim$ 3.45 to 4.1 km/s as the Moho, whereas <u>Finotello, et</u>
1776	al. [2011] associated the Moho with a velocity jump from 4.1 to 4.45 km/s. It is well
1777	known that the Moho represents a sharp increase from a low velocity in the crust to a
1778	high velocity in upper mantle. However, during the procedure of inverting 1D
1779	S-velocities from receiver functions, vertical smearing or smoothing will result in a
1780	lower S-velocity at the real Moho position in the inverted model than the real structure.
1781	As such, it is reasonable to select a velocity slightly lower than expected for the upper
1782	mantle to represent the velocity at the Moho position. Furthermore, the velocity
1783	increase with depth from 3.45 to 4.1 km/s in Lawrence, et al. [2006] is sharper than
1784	that from 4.1 km/s to 4.45 km/s, which indicates that the Moho position is at the
1785	shallower of the two estimates. For a complex crustal structure like that beneath CBOB,
1786	the assumption of both a constant Vp and single layer model used in the $H-\kappa$ stacking
1787	method may be too simplistic, and can result in a large uncertainty on the calculated
1788	crustal thickness. For example, S-velocity models beneath SBA [Bannister, et al., 2003]
1789	show that Vs gradually increases from 1.2 to 4.3 km/s down to 20 km, which implies
1790	that Vp is also gradually increasing through these depths. In this case, a constant Vp

- 1791 and single layer model used in the  $H-\kappa$  stacking method may not adequately represent
- the structure beneath SBA. Receiver functions from different studies [Bannister, et al.,
- 1793 2003; Lawrence, et al., 2006; Finotello, et al., 2011] are similar and provide a similar
- time difference between Ps and P of ~4 s. However, *Finotello, et al.* [2011] calculated a
- 1795 27 km deep Moho by the  $H-\kappa$  stacking method, and S-velocity models inverted by two
- 1796 different global algorithms by *Bannister, et al.* [2003] and *Lawrence, et al.* [2006] both
- 1797 yielded different thickness of ~21 km. Similar issues can also be identified for other
- 1798 stations, such as CBOB, CTEA, CCRZ (CCRI in Table 1 of *Lawrence, et al.* [2006],
- and MAGL. For the above reasons, we discarded the Moho depths from *Finotello, et al.*
- 1800 [2011] and those obtained using S-velocity model inversions in other studies.
- 1801
- 1802 For the SNAA station, *Bayer, et al.* [2009] obtained a 41-km-thick crust, corresponding
- 1803 to a high Vp/Vs from the  $H-\kappa$  method, and also calculated a 39-km-thick crust from
- 1804 the time difference between Ps and P. We used the mean of the two thicknesses (40
- 1805 km), which is also the Moho depth estimated from short-period (2–12 s) signals [see
- 1806 Table 4 in *Bayer, et al.*, 2009]. The Moho depth of 52 km for MUCs is from MUC6–8
- 1807 stations and of 45 km for AWIs is from AWI2–4 of fig. 10 in *Bayer, et al.* [2009].
- 1808
- 1809 The names of some positions have been modified according to the information in 1810 original publications. J99-S1 to J99-S6 are shot points from S1 to S6, respectively, of
- 1811 the 41<sup>st</sup> Japanese Antarctic Research Expedition (JARE41) in the austral summer of

1812 1991–2000 [Yoshii, et al., 2004], and J01-SPs are SP1–SP7 of JARE43 in the 2001–

- 1813 2002 season [Miyamachi, et al., 2003]. J01-SP3 and 4 were discarded because the
- 1814 locations are too close and give the same Moho depth as J99-S3. WA-As or WA-Bs are
- 1815 sections A and B, respectively, from the Wilkes–Adelie margin of Antarctica [*Eittreim*,
- 1816 <u>1994</u>]. M450 is the mid-point between shots 45 and 50 of the reflection profile
- 1817 from[*McGinnis, et al.*, 1985]. The numbers for the points from D000 to D780 represent
- 1818 the distance along the profile in fig. 5 of *Leitchenkov and Kudryavtzev* [1997]. RIS51
- 1819 and 56 are stations 51 and 56 on the Ronne Ice shelf from *Jokat, et al.* [1997]. Fisher is
- 1820 the FISH station from Reading [2006].
- 1821

1822 On the basis of the above corrections and selection criteria, we compiled the AN-Moho 1823 (Figure S7c) and Moho depths listed in Table S1. Apart from the crustal thickness of 1824 Dome F (Figure S7a) obtained from gravity data in Kanao, et al. [2012], no valid data 1825 from seismic methods is yet available for Queen Maud Land (QML), Dome F, and 1826 Ellsworth Land (EL). In our compilation, most of the Moho points in the AN-Moho are located on the Antarctic continent. The thickest crust is found beneath Dome A, where 1827 1828 it is as thick as ~61.6 km, whereas the Moho is 57.5 km below sea level. For oceanic 1829 regions, the oceanic crust is generally thin (average thickness, ~6 km; [McClain and 1830 Atallah, 1986]. However, several measurements of oceanic crustal thickness around 1831 Antarctica where ocean depths are >3 km have shown that the crustal thickness varies 1832 in the range of 7–20 km. Therefore, the oceanic crustal structure around Antarctica is

1833	complex.
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1987	Caption of supplementary table:
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1989	Table S1. Crustal thicknesses in the compilation of AN-Moho
1990	(This table can be found in "01 Seismic model_ANT_v12_suppl_Table
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## 1995 **Captions of supplementary figures:**

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1997 Figure S1 Illustration of the progressive formation of Gondwana and Pangaea. The 1998 formation steps of Gondwana in (a, b) are simplified from [Boger, 2011]. The 1999 reconstruction of Pangaea in (c) is from [*Schettino and Scotese*, 2005]. AF = African 2000 continent; AU = Australian continent; EANT = East Antarctica; IN = Indian continent; 2001 SA = South American continent. A red circle labeled with "A" marks the position of Dome Argus of the GSM, which is the highest ice feature in Antarctica. Three 2002 2003 rectangles labeled with a number highlight typical areas of EANT which were 2004 respectively parts of three continents (1: West Gondwana; 2: Indo-Antarctica; 3: East 2005 Gondwana). Blue arrows indicate the movement or rotation of the continent. The block shaded by yellow color has not been geologically studied. Red dashes in (b) 2006 2007 indicatively mark suture zone of the amalgamation of the three continents, and in (c) 2008 mark the boundary of Gondawana.

2009

Figure S2 Illustration of the evolution of Gondwana during the past 160 Ma. AF = African continent; AP = Antarctic Peninsular; AUS = Australian continent; BaH = Balleny hotspot; BH = Bouvet hotspot; EANT = East Antarctica; IN = Indian continent; KH = Kerguelen hotspot; MH = Marion hotspot; SA = South American continent. The continental reconstructions and the locations of LIPs are from [*Schettino and Scotese*,

2016 <u>2005</u>]. The subduction zones shown in panels (a) to (c) are adapted from [*Torsvik, et al.*,

- 2017 <u>2008a</u>], and in (d) are from [*Breitsprecher and Thorkelson*, 2009]. The hotspots of BH,
- 2018 MH, and KH are from [*Torsvik, et al.*, 2008a].

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Figure S3. Resolution length information for Rayleigh wave dispersions at periods of (a-c) 50 s, (d) 100 s, and (e) 150 s. Plate (b) shows the inverted solution for a synthetic model in (a) at a period of 50 s. The resolution length maps (c-e) were retrieved from 400 pairs of random synthetic models and their solutions. The propagation paths used to estimate the resolution lengths in (c-e) are the same as those in Figure 3b-d.

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Figure S4. The 3D S-velocity solutions directly inverted from the synthetic observations of random synthetic models. (a) is a slice of a random synthetic model at a depth of 50 km. (b) and (c) are slices at depths of 50 and 120 km, respectively and (e) and (f) are vertical slices along two transects, respectively, however, the slices and transects are from the same solution inverted from the synthetic 3D model shown in (a). (d) is a slice at a depth of 200 km from a solution on the basis of another random synthetic model.

Figure S5. Fundamental-mode Rayleigh wave group velocity (U) sensitivity with
respected to vertical S-velocity (β) variation at depth. The sensitivities are calculated
on the basis of IASPEI91 model [Kennett and Engdahl, 1991].

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2042	Figure Se	5. Two	3D	models	from	inversions	with	and	without	Moho	constraints	in	the

2043 last iteration. The 1D profiles in (b) are beneath the same position labeled with "t" in

2044 (a), in which the position of the transect A-A' in (c) and (d) is also shown. The symbols

2045 in (c,d) are the same as those in Figure 7.

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Figure S7. Moho depths. (a) Positions (plus symbol) of Moho depths from previous studies. (b) Moho depths with a difference of >2 km at a given position. The points surrounded by black lines were used in the AN-Moho model. (c) Moho depths in the compilation of AN-Moho for Antarctica. All the Moho depths and the previous studies that the Moho depths come from are listed in Table S1.

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Table S1 Crustal thicknesses in the compilation of AN-Moho

Name	Longitude (°)	Latitude (°)	Crustal thickness (km)	Moho depths (km)	Sources
9169	-6.02	-75	45.0	42.3	1
9172	-9.7	-73.6	44.0	42.6	1
96100B	5.9	-67.7	12.0	16.0	2
96100E	6.1	-69.7	23.0	25.0	2
96110B	-14.1	-69	10.0	14.0	2
96110E	-12.5	-73.5	21.0	23.0	2
А	67	-72	32.0	32.0	<u>3,4</u>
AMERY	73.85	-69.71	30.0	30.0	<u>3,4</u>
AN01	166.92	-77.19	20.0	19.8	5
AN05	163.96	-77.69	18.0	17.8	5
AN08	160.15	-77.54	40.0	37.9	5
AN09	162.17	-77.93	34.0	32.8	5
AN10	162.83	-77.63	32.0	31.3	5
AWI2-4	-13.09	-74.5	45.9	45.0	<u>6</u>
В	78.2	-68.77	34.0	34.0	<u>3.4</u>
BEAVER	68.34	-70.75	30.0	30.0	<u>3,4</u>
BT01	166.563	-71.112	25.0	23.3	2
BT05	158.928	-69.89	31.0	29.5	2
BT06	157.337	-69.514	32.0	31.4	2
BT07	155.03	-69.245	31.0	30.0	2
BVLK	68.17	-70.8	33.0	32.9	<u>8</u>
BYRD	-119.473	-80.0168	26.75	25.2	2
BYRD	-119.5466	-80	27.0	25.5	<u>10</u>
С	69.09	-71.55	24.0	24.0	<u>3.4</u>
CASE	160.1262	-80.4481	27.8	27.0	<u>11</u>
CASEY	110.31	-66.17	30.0	30.0	<u>12</u>
CBOB	163.1707	-77.0342	20.1	20.0	<u>11</u>
CBRI	166.4266	-77.2516	18.3	18.0	ш
CCRZ	169.0947	-77.5166	19.8	19.0	ш
CHNA	77.013	-78.677	46.8	43.3	<u>13</u>
CHNB	76.976	-77.1744	57.5	54.5	<u>13</u>
CLRK	-141.8485	-77.3231	30	29.0	2
CPHI	162.6484	-75.0745	22.2	22.0	<u>11</u>
CRES	64.17	-72.66	33.0	31.6	<u>8</u>
CTEA	160.7643	-78.9439	21.3	20.0	<u>11</u>
D000	298.5	-74.86	37.0	37.0	14
D100	301	-75.45	35.0	35.0	<u>14</u>
D200	304	-76.06	33.0	33.0	<u>14</u>
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D320	-52.5	-76.8	32.0	32.0	<u>14</u>
D420	-49	-77.2	30.0	30.0	<u>14</u>
D500	-47	-77.7	29.0	29.0	<u>14</u>
D640	-41	-77.8	32.0	32.0	<u>14</u>
D	72.38	-69.49	24.0	24.0	<u>3,4</u>
D780	-36	-77.8	41.0	41.0	<u>14</u>
DAVI	78	-68.7	39.0	38.9	<u>8</u>
DEVL	161.9745	-81.4757	18	17.9	2
DIHI	159.48	-79.8491	21.4	21.0	<u>11</u>
DNTW	-107.7804	-76.4571	25.21	24.2	2
DOMEA	77.1047	-80.422	61.6	57.5	<u>13</u>
DRV	140	-66.8	28.0	27.6	<u>15</u>
DSS2	-59.5	-62.5	33.0	32.9	<u>16</u>
DSS6	-62.5	-64.7	35.0	34.4	<u>16</u>
DT154	77.0257	-74.5824	49.3	46.6	<u>13</u>
DUFK	-53.2007	-82.8619	38.4	37.4	2
E000	163.6175	-77.6262	20.3	20.0	Ш
E002	163.0078	-77.575	24.7	24.0	Ш
E004	162.0661	-77.4133	30.7	30.0	<u>11</u>
E006	161.6256	-77.3703	34.6	34.0	<u>11</u>
E008	160.5033	-77.2817	37.8	36.0	<u>11</u>
E010	160.086	-77.1847	39.0	37.2	<u>17,18</u>
E012	159.326	-77.0461	40.6	38.7	<u>18</u>
E018	157.224	-76.8234	40.7	38.6	<u>18</u>
E020	156.547	-76.7295	45.2	43.0	<u>18</u>
E024	155.238	-76.5394	45.6	43.4	<u>18</u>
E028	154.039	-76.3075	45.6	43.3	<u>18</u>
E030	153.379	-76.2511	45.5	43.2	<u>18</u>
EAGLE	77.0448	-76.4154	58.4	55.6	<u>13</u>
ERS11	-174.445	-77.12	17.5	18.0	<u>19</u>
ERS13	-173.637	-77.1217	17.5	18.0	<u>19</u>
ERS17	-172.027	-77.1217	18.5	19.0	<u>19</u>
ERS20	-170.813	-77.1217	19.5	20.0	<u>19</u>
ERS23	-169.61	-77.1217	21.5	22.0	<u>19</u>
ERS3	-178.583	-77.12	23.4	24.0	<u>19</u>
ERS5	-176.99	-77.1167	23.4	24.0	<u>19</u>
ESPZ	301.6	-63.7	37.0	36.4	<u>20</u>
FALL	-143.6284	-85.3066	24	23.7	<u>9</u>
FISH	162.5652	-78.9276	17	16.7	2
FISHER	67.39	-71.52	39.0	38.4	<u>8</u>
GM01	104.7291	-83.9858	34.5	31.2	<u>21</u>
GM02	97.5815	-79.4251	42.3	38.6	<u>21</u>
GM03	85.9439	-80.2169	56.0	52.1	21

GM04	61.1124	-82.9997	51.5	47.7	<u>21</u>
GM05	51.1588	-81.1841	50.2	46.4	<u>21</u>
GROV	75	-72.9	40.0	38.0	<u>8</u>
HOWD	-86.7694	-77.5285	37	35.5	<u>9</u>
ISDE	-134.9935	-80	28.0	27.4	<u>10</u>
J01-SP1	41.2	-70.2	41.0	40.0	<u>22</u>
J01-SP2	41.5	-69.8	41.0	40.0	<u>22</u>
J01-SP5	42.4	-69.25	41.0	40.0	<u>22</u>
J01-SP6	42.7	-69.08	41.0	40.0	<u>22</u>
J01-SP7	42.95	-68.7	41.0	40.0	<u>22</u>
J99-S1	40.06	-69.04	38.0	37.0	<u>23</u>
J99-S2	40.65	-69.06	40.0	39.0	<u>23</u>
J99-S3	41.3	-69.3	41.0	40.0	<u>23</u>
J99-S4	42	-69.6	42.0	41.0	<u>23</u>
J99-S5	42.6	-69.8	43.5	42.0	<u>23</u>
J99-S6	43.4	-70.2	45.0	43.0	<u>23</u>
JNCT	157.901	-76.9313	38.0	35.8	<u>18</u>
LONW	152.735	-81.3466	45	43.5	<u>9</u>
LT892	77.767	-71.6708	45.7	43.5	<u>13</u>
M450	165.4	-77.75	21.0	21.0	<u>24</u>
MAGL	162.4083	-76.1381	23.0	23.0	ш
MBL	-130.2241	-78.093	25.0	23.4	<u>10</u>
MECK	-72.1849	-75.2807	26.5	25.4	2
MILR	156.2517	-83.3063	45	43.1	<u>9</u>
MINN	166.88	-78.5504	20.5	20.0	<u>11</u>
MPAT	-155.022	-78.0297	27.5	27.0	<u>9</u>
MTM	-100.0123	-79.496	21.0	19.0	<u>10</u>
MUC6-8	-11.065	-75.25	53.1	51.0	<u>6</u>
MZH	44.3	-70.1	44.0	42.0	<u>23,25</u>
N000	160.378	-76.0088	32.8	31.1	<u>18</u>
N020	155.818	-77.4678	40.5	38.2	<u>18</u>
N036	151.278	-78.5508	44.0	41.7	<u>18</u>
N044	148.616	-79.0692	47.0	44.7	<u>18</u>
N060	142.595	-80.0001	47.9	45.5	<u>18</u>
N076	135.434	-80.8062	48.0	45.5	<u>18</u>
N092	126.98	-81.4593	46.6	43.8	<u>18</u>
N100	122.61	-81.6525	45.5	42.6	<u>18</u>
N108	117.605	-81.8795	47.0	43.9	<u>18</u>
N116	112.571	-82.0098	45.1	41.9	<u>18</u>
N124	107.6406	-82.0745	47.9	44.5	<u>21</u>
N132	101.9534	-82.0751	45.3	41.9	<u>21</u>
N140	96.7692	-82.0086	49.3	45.7	<u>21</u>
N156	86.5045	-81.6726	46.3	42.4	<u>21</u>

N165	81.7604	-81.4084	56.5	52.5	<u>21</u>
N173	77.4736	-81.1122	59.2	55.2	<u>21</u>
N182	73.1898	-80.7363	57.8	53.7	<u>21</u>
N190	69.431	-80.3275	51.5	47.6	<u>21</u>
N198	65.9607	-79.8597	53.4	49.6	<u>21</u>
N206	62.8556	-79.3947	50.3	46.6	<u>21</u>
N215	59.9943	-78.9045	47.9	44.4	<u>21</u>
NOVO	11.835	-70.776	42.0	41.8	<u>6</u>
OND	-125.7358	-80.7456	28.0	26.9	<u>10</u>
P061	77.2238	-84.4996	46.1	42.6	<u>21</u>
P071	77.3347	-83.6465	43.0	39.4	<u>21</u>
P080	77.364	-82.8054	48.0	44.2	<u>21</u>
P116	77.0451	-79.5669	56.7	52.8	<u>21</u>
P124	77.657	-78.8718	58.9	55.3	<u>21</u>
PECA	-68.5527	-85.6124	37	35.5	2
PMSA	296	-64.8	40.0	39.8	<u>20</u>
**PMSA	-64	-64.8	36.0	36.0	<u>15</u>
REIN	72.55	-70.45	33.0	32.9	<u>8</u>
RIS51	-61	-74.7	33.0	33.0	<u>26</u>
RIS56	-55	-75.8	27.0	27.0	<u>26</u>
SAE33B	-12.5	-71.5	32.0	32.0	<u>6,27</u>
SAE33E	-7.2	-70.7	32.0	32.0	<u>6,27</u>
SAE34B	-10.5	-71	33.0	33.0	<u>6,27</u>
SAE34E	-4.8	-73.4	41.0	39.0	<u>6,27</u> , <u>1</u>
SBA	166.7573	-77.8491	21.0	21.0	ш
SBA	166.757	-77.8491	21.0	21.0	<u>5</u>
SDM	-148.85	-81.6148	27.0	26.3	<u>10</u>
SILY	-125.966	-77.1332	32.8	30.7	<u>9</u>
SIPL	-148.9555	-81.6405	28.03	27.4	<u>9</u>
SNAA	-2.838	-71.671	40.0	39.2	<u>6</u>
SPA	0	-90	34.0	31.2	<u>10</u>
ST01	-98.7419	-83.2279	30.24	28.2	<u>9</u>
ST02	-109.1243	-82.069	34.24	32.5	<u>9</u>
ST03	-113.1504	-81.4065	26.53	24.9	<u>9</u>
ST04	-116.5782	-80.715	23.76	22.2	<u>9</u>
ST06	-121.8196	-79.3316	24.8	23.3	<u>9</u>
ST07	-123.7953	-78.6387	26.21	24.6	<u>9</u>
ST08	-125.5313	-77.9576	26.8	25.0	<u>9</u>
ST09	-128.4734	-76.5309	31.74	29.5	2
ST10	-129.7489	-75.8143	29.83	28.1	2
ST12	-123.816	-76.897	24.02	21.8	<u>9</u>
ST13	-130.5139	-77.5609	32.18	30.3	2
ST14	-134.0802	-77.8378	28.93	27.3	2
					-

STC-136.4061-82.37531.030.5 $!!!SURP-171.2018-84.71926.526.10?THUR-97.5060-72.50121.1023.0011TNV164.12-74.722.3921.10?UPTW-109.0396-77.57923.3035.0012**VNDA161.846-77.51335.6036.404.3**VNDA161.850-77.51235.3034.7012**VNDA161.853-77.51235.3036.7027VOSTOK106.48-78.2830.0026.5027**VNDA161.853-78.2830.0026.5027WA-MN131.5-6418.021.0027WA-MN131.5-64.110.601227WA-MN141-65.110.0118.7027WA-BN141-65.110.0118.7021WA-BN141-65.110.011221WA-BN141-65.110.0112WA-BN141-65.131.5031.6121WA-BN141-65.110.011221WA-BN141-65.110.0121WA-BN141-65.131.5031.6121WA-BN141-65.131.5031.6121WA-BN141-65.131.5032.6121WA-BN141-65.131.6132.6121$						
SURP.171.2018.84.719926.526.1.22THUR.97.5606.72.530124.123.9.2.1TNV164.12.74.721.122.0.1.1UPTW.100.0396.77.579723.3031.1.2.1**NDA161.845.77.513935.034.4.1.1**VNDA161.846.75.17235.334.7.1.1**VNDA161.853.77.517235.334.7.1.1VOSTOK106.48.78.2830.026.5.2.1**VOSTO106.48.78.2835.031.5.2.1WA-M131.5.6418.021.0.8.1WA-M131.5.6416.018.7.2.1WA-BM141.65.116.018.7.2.1WA-BM141.65.623.024.1.2.2WAIS.111.7776.94.1825.5723.8.2.1WIT.104.3867.82.682331.530.2.2.1WITS.80.5587.80.039630.2.2.2.2WITS.152.4.71.4150.047.4.6.1WITS.152.4.71.43745.043.6.2.1WITS.152.4.71.13745.043.6.2.2WITS.152.4.71.13715.515.0.2.2W	STC	-136.4061	-82.3575	31.0	30.5	<u>10</u>
THUR.97.5606.72.530124.123.9?TNV164.12.74.722.122.011UPTW.109.0396.77.579722.3921.1?WNDA161.8450.77.513935.635.014**VNDA161.8450.77.513935.034.4.512**VNDA161.8450.77.517235.334.716VOSTOK106.48.78.2830.026.526**VOSTO106.48.78.2835.031.527KWA-M13.5.64.118.021.029WA-M13.5.64.116.018.729WA-BN141.65.116.018.729WA-BN141.65.623.024.129WA-BN141.65.623.024.129WA-BN11.776.79.418125.5723.82WILS.96.22.74.27544.042.52WHT.104.3867.82.682331.530.22WILS.80.5587.80.03963029.32WNA11.524.77.14345.043.64WHT.11.784.77.13745.043.62WHT.11.524.77.14153.11.02WRS1.11.524.77.13715.515.014WRS1.11.525.77.10515.515.0	SURP	-171.2018	-84.7199	26.5	26.1	2
TNV164.12-74.722.122.011UPTW-109.0396-77.579722.3921.1?VNDA161.8450-77.513935.635.011**VNDA161.846-77.513935.034.4517**VNDA161.853-77.517235.334.718VOSTOK106.48-78.2830.026.526**VOSTO106.48-78.2835.031.527KWA-M13.5-6418.021.029WA-M13.5-6416.018.729WA-M13.5-6416.018.729WA-M14.1-65.116.018.729WA-BN14.1-65.623.024.129WA-BN14.1-65.623.024.129WA-BN11.1776-79.418125.5723.82WILS-9.622-74.27544.042.52WILS-80.587-80.03630.22.32WILS-80.587-80.03630.22.32WILS-11.7169-72.0451.048.62WND11.524-71.03745.043.62WRS10-172.788-77.07118.519.02WRS11-172.786-77.07516.517.02WRS12-176.26-77.105123.424.02 <td< td=""><td>THUR</td><td>-97.5606</td><td>-72.5301</td><td>24.1</td><td>23.9</td><td>2</td></td<>	THUR	-97.5606	-72.5301	24.1	23.9	2
UPTW.109.0390.7.73792.2.392.1.1?VNDA161.8450.7.7.5139.5.6.35.0.11**VNDA161.843.7.7.5132.5.3.3.4.1.5.7**VNDA161.853.7.7.5172.5.3.3.4.7.15**VOSTOK106.48.7.8.28.30.0.26.5.2**VOSTOK106.48.7.8.28.5.0.1.5.2**VOSTO10.6.48.7.8.28.5.0.1.5.2**VOSTO10.6.48.6.1.1.0.1.1.2WA-AM.1.1.6.1.1.0.1.1.2WA-BM.1.1.6.1.1.0.1.1.2WA-BM.1.1.6.1.7.0.1.6.2WA-BM.1.1.6.1.7.0.1.1.2WA-BM.1.1.77.7.9.18.2.5.2.3.2WA-BM.1.1.77.7.4.18.2.5.2.3.2WIT.1.0.3.807.8.0.390.3.1.3.1.2WIT.1.0.4.387.8.0.390.3.1.3.1.2WIT.1.0.4.387.2.144.5.1.3.1.2WIT.1.0.4.387.2.144.5.1.3.1.2WIT.1.0.4.387.2.144.5.1.3.1.2WIT.1.0.4.387.2.144.5.1.3.1.2WIT.1.0.4.387.5.14.5.1.3.1.2WIT.1.5.2.7.141.5.1.3.1.2WIT<	TNV	164.12	-74.7	22.1	22.0	<u>11</u>
NNDA161.8450.77.513935.635.0 $!!$ **VNDA161.853.77.517235.334.4 $!!$ **VNDA161.853.77.517235.334.7 $!!$ VOSTOK106.48.78.2830.026.5 $!!$ **VOSTO106.48.78.2835.0.15.0 $!!$ WA-AM131.5.6418.021.0 $!!$ WA-AM131.5.6418.016.3 $!!$ WA-BM141.65.116.018.7 $!!$ WA-BN141.65.123.024.1 $!!$ WA-BN141.65.623.024.1 $!!$ WA-BS.111.776.79.418125.5723.8 $!!$ WHIE.96.22.74.27544.042.5 $!!$ WHIT.104.867.82.682331.530.2 $!!$ WHIT.104.867.82.682331.530.2 $!!WHI2.15.24.71.41450.047.4!<$	UPTW	-109.0396	-77.5797	22.39	21.1	<u>9</u>
**VNDA161.846.77.51935.034.44.17**VNDA161.853.77.517235.334.718VOSTOK106.48.78.2830.026.522**VOSTO106.48.78.2835.031.522**VOSTO106.48.78.2835.031.521WA-AM131.5.6418.021.039WA-AM132.63.212.016.339WA-BM141.65.116.018.729WA-BM141.65.623.024.129WA-BS141.65.623.024.129WA-BS141.65.623.024.129WA-BS.111.776.79.41825.5723.82WAIS.111.776.79.41825.5730.22WHT.104.3867.82.682331.530.22WHT.104.3867.82.682331.530.22WHT.1052.71.43745.043.62WN7311.562.71.43745.043.62WN7411.94129.82.369523.1722.21WR510.172.386.77.07118.519.012WR511.172.155.77.05516.517.012WR512.176.20.14.924.0122WR514.174.05.77.15515.516.012WR515.179.91.55.116.	VNDA	161.8456	-77.5139	35.6	35.0	<u>11</u>
**VNDA161.853.77.51235.334.7.8VOSTOK106.48.78.2830.026.5.2**VOSTO106.48.78.2835.031.5.2K.7WA-AM131.5.6418.021.0.2WA-AM132.63.212.016.3.2WA-BM141.65.116.018.7.2WA-BN141.64.17.010.6.2WA-BN141.65.623.024.1.2WA-BS.111.776.79.41825.5723.8.2WEIGEL.9.622.74.27544.042.5.2WHT.104.3867.82.682331.5.30.2.2WHT.104.3867.82.682331.5.30.2.2WHT.104.3867.82.682331.5.30.2.2WHT.104.3867.82.682331.5.30.2.2WHT.104.3867.82.682331.5.30.2.2WHT.104.3867.72.1450.0.47.4.2WM7211.524.71.43745.0.43.6.2WN7311.524.71.43745.0.36.1.2WN51.172.386.77.07118.519.0.2WR51.172.154.77.05516.5.16.0.2WR51.175.15.77.16513.516.0.2WR51.176.82.77.105123.4 <td>**VNDA</td> <td>161.846</td> <td>-77.5139</td> <td>35.0</td> <td>34.4</td> <td><u>5,17</u></td>	**VNDA	161.846	-77.5139	35.0	34.4	<u>5,17</u>
VOSTOK         106.48         -78.28         30.0         26.5         2           **VOSTO         106.48         -78.28         35.0         31.5         2           K         -         -64         18.0         21.0         3           WA-AM         131.5         -64         18.0         16.3         3           WA-BM         141         -65.1         16.0         18.7         3           WA-BN         141         -65.6         23.0         24.1         3           WA-BS         141         -65.6         23.0         24.1         3           WAIS         -111.776         -79.4181         25.57         23.8         2           WIS         -114.3867         82.6823         31.5         30.2         2           WILS         -80.587         -80.0306         30         29.3         2           WM72         11.524         -72.144         50.0         47.4         6           WM73         11.562         -71.437         45.0         48.6         9           WM74         119.4129         -82.3695         23.17         22.2         2           WR510         -172.386	**VNDA	161.853	-77.5172	35.3	34.7	<u>18</u>
**VOSTO106.48-78.2855.031.522KWA-AM131.5-6418.021.030WA-AM132-63.212.016.330WA-BM141-65.116.018.730WA-BN141-65.623.024.130WA-BS141-65.623.024.130WAIS-111.776-79.41825.5723.82WEIGEL-9.622-74.27544.042.52WHT-104.3867-82.682331.530.22WHT1.524-72.14450.047.46WM7311.562-71.43745.043.66WM74119.129-82.369523.1722.22WR51-172.386-77.01718.519.012WRS1-174.005-77.10513.514.012WRS1-175.215-77.10513.514.012WR51-179.30315.516.012WR52-179.33123.424.012WR51-179.33123.424.012WR52-179.33155.716.517.0WR52-179.33123.424.012WR53-169.618-77.101823.424.012WR54-169.986-77.10123.424.012WR54-169.986-77.10115.516.0	VOSTOK	106.48	-78.28	30.0	26.5	<u>28</u>
K         Interpretation         Interpretation         Interpretation           WA-AM         131.5         -64         18.0         21.0         Image: Interpretation           WA-AM         132         -63.2         12.0         16.3         Image: Interpretation           WA-BM         141         -65.1         16.0         18.7         Image: Interpretation           WA-BN         141         -64.1         7.0         10.6         Image: Interpretation           WA-BN         141         -65.6         23.0         24.1         Image: Interpretation           WA-BN         -111.776         -79.4181         25.57         23.8         Image: Interpretation           WAIS         -111.776         -79.4181         25.57         30.2         Image: Interpretation           WHIT         -104.3867         -82.6823         31.5         30.2         Image: Interpretation           WILS         -80.5587         -80.0396         30         29.3         Image: Interpretation           WIT2         11.524         -71.437         45.0         43.6         Image: Interpretation           WN73         11.525         -71.037         18.5         19.0         Image: Interpretation	**VOSTO	106.48	-78.28	35.0	31.5	<u>29</u>
WA-AM         131.5         -64         18.0         21.0         20           WA-AN         132         -63.2         12.0         16.3         30           WA-BM         141         -65.1         16.0         18.7         30           WA-BN         141         -64.1         7.0         10.6         20           WA-BS         141         -65.6         23.0         24.1         20           WAIS         -111.7776         -79.4181         25.57         23.8         2           WEIGEL         -9.622         -74.275         44.0         42.5         6           WHT         -104.3867         -82.6823         31.5         30.2         2           WILS         -80.5587         -80.0396         30         29.3         2           WM72         11.524         -72.144         50.0         47.4         6           WM79         13.215         -72.04         51.0         48.6         6           WN79         13.215         -77.0717         18.5         19.0         19           WRS10         -172.386         -77.0755         16.5         17.0         19           WRS11         -172.03 <td>К</td> <td></td> <td></td> <td></td> <td></td> <td></td>	К					
WA-AN         132         -63.2         12.0         16.3         29           WA-BM         141         -65.1         16.0         18.7         29           WA-BN         141         -64.1         7.0         10.6         29           WA-BS         141         -65.6         23.0         24.1         29           WAIS         -111.7776         -79.4181         25.57         23.8         2           WEIGEL         -9.622         -74.275         44.0         42.5         6           WHT         -104.3867         -82.6823         31.5         30.2         2           WILS         -80.5587         -80.0396         30         29.3         2           WM72         11.524         -72.144         50.0         47.4         6           WM73         11.562         -71.437         45.0         48.6         6           WN74         11.215         -72.04         51.0         48.6         6           WN51         -172.386         -77.0717         18.5         19.0         12           WRS11         -172.788         -77.1055         15.0         12           WRS14         -176.026         -	WA-AM	131.5	-64	18.0	21.0	<u>30</u>
WA-BM         141         -65.1         16.0         18.7         3º           WA-BN         141         -64.1         7.0         10.6         3º           WA-BS         141         -65.6         23.0         24.1         3º           WAIS         -111.7776         -79.4181         25.57         23.8         ?           WEIGEL         -9.622         -74.275         44.0         42.5         \$           WHT         -104.3867         -82.6823         31.5         30.2         ?           WILS         -80.5587         -80.0396         30         29.3         ?           WM72         11.524         -72.144         50.0         47.4         \$           WM73         11.562         -71.437         45.0         43.6         \$           WM79         13.215         -72.04         51.0         48.6         \$           WN51         -119.4129         -82.3695         23.17         22.2         ?           WRS10         -172.386         -77.0717         18.5         19.0         12'           WRS11         -172.788         -77.1055         15.5         16.0         12'           WRS12	WA-AN	132	-63.2	12.0	16.3	<u>30</u>
WA-BN         141         -64.1         7.0         10.6         B           WA-BS         141         -65.6         23.0         24.1         B           WAIS         -111.7776         -79.4181         25.57         23.8         2           WEIGEL         -9.622         -74.275         44.0         42.5         6           WHT         -104.3867         -82.6823         31.5         30.2         2           WILS         -80.5587         -80.0396         30         29.3         2           WM72         11.524         -72.144         50.0         47.4         6           WM73         11.562         -71.437         45.0         43.6         6           WM74         11.94129         -82.3695         23.17         22.2         2           WRS10         -172.386         -77.0717         18.5         19.0         12           WRS11         -172.788         -77.0755         16.5         17.0         12           WRS12         -173.203         -77.1052         20.4         21.0         12           WRS14         -174.005         -77.1051         23.4         24.0         12           WRS21 <td>WA-BM</td> <td>141</td> <td>-65.1</td> <td>16.0</td> <td>18.7</td> <td><u>30</u></td>	WA-BM	141	-65.1	16.0	18.7	<u>30</u>
WA-BS         141         -65.6         23.0         24.1         22           WAIS         -111.7776         -79.4181         25.57         23.8         2           WEIGEL         -9.622         -74.275         44.0         42.5         6           WHIT         -104.3867         -82.6823         31.5         30.2         2           WILS         -80.5587         -80.0396         30         29.3         2           WM72         11.524         -72.144         50.0         47.4         6           WM73         11.562         -71.437         45.0         43.6         6           WM79         13.215         -72.04         51.0         48.6         6           WNDY         -119.4129         -82.3695         23.17         22.2         2           WRS10         -172.386         -77.0717         18.5         19.0         19           WRS11         -172.788         -77.0755         16.5         17.0         19           WRS12         -173.203         -77.0892         14.5         15.0         19           WRS14         -174.005         -77.1051         23.4         24.0         19           W	WA-BN	141	-64.1	7.0	10.6	<u>30</u>
WAIS         -111.7776         -79.4181         25.57         23.8         2           WEIGEL         -9.622         -74.275         44.0         42.5         6           WHIT         -104.3867         -82.6823         31.5         30.2         2           WILS         -80.5587         -80.0396         30         29.3         2           WM72         11.524         -72.144         50.0         47.4         6           WM73         11.562         -71.437         45.0         43.6         6           WM79         13.215         -72.04         51.0         48.6         6           WNDY         -119.4129         -82.3695         23.17         22.2         2           WRS10         -172.386         -77.0717         18.5         19.0         19           WRS11         -172.788         -77.055         16.5         17.0         19           WRS12         -173.203         -77.052         20.4         21.0         19           WRS14         -174.005         -77.1051         23.4         24.0         19           WRS2         -169.226         -77.039         15.5         16.0         19           <	WA-BS	141	-65.6	23.0	24.1	<u>30</u>
WEIGEL       -9.622       -74.275       44.0       42.5       9         WHIT       -104.3867       -82.6823       31.5       30.2       9         WILS       -80.5587       -80.0396       30       29.3       9         WM72       11.524       -72.144       50.0       47.4       6         WM73       11.562       -71.437       45.0       43.6       6         WM79       13.215       -72.04       51.0       48.6       9         WNDY       -119.4129       -82.3695       23.17       22.2       9         WRS10       -172.386       -77.0717       18.5       19.0       19         WRS11       -172.788       -77.0755       16.5       17.0       19         WRS12       -173.203       -77.0892       14.5       15.0       19         WRS14       -174.005       -77.1055       13.5       14.0       19         WRS21       -176.826       -77.1051       23.4       24.0       19         WRS2       -169.226       -77.1051       23.4       24.0       19         WRS2       -169.26       -77.1051       23.4       24.0       19 <t< td=""><td>WAIS</td><td>-111.7776</td><td>-79.4181</td><td>25.57</td><td>23.8</td><td>2</td></t<>	WAIS	-111.7776	-79.4181	25.57	23.8	2
WHIT       -104.3867       -82.6823       31.5       30.2       2         WILS       -80.5587       -80.0396       30       29.3       2         WM72       11.524       -72.144       50.0       47.4       6         WM73       11.562       -71.437       45.0       43.6       6         WM79       13.215       -72.04       51.0       48.6       6         WNDY       -119.4129       -82.3695       23.17       22.2       2         WRS10       -172.386       -77.0717       18.5       19.0       19         WRS11       -172.788       -77.0755       16.5       17.0       19         WRS12       -173.203       -77.0892       14.5       15.0       19         WRS14       -174.005       -77.1055       13.5       14.0       19         WRS17       -175.215       -77.1052       20.4       21.0       19         WRS2       -169.226       -77.1051       23.4       24.0       19         WRS2       -169.226       -77.1051       23.4       24.0       19         WRS2       -169.618       -77.1018       16.5       17.0       19	WEIGEL	-9.622	-74.275	44.0	42.5	<u>6</u>
WILS       -80.5587       -80.0396       30       29.3       2         WM72       11.524       -72.144       50.0       47.4       6         WM73       11.562       -71.437       45.0       43.6       6         WM79       13.215       -72.04       51.0       48.6       6         WNDY       -119.4129       -82.3695       23.17       22.2       9         WRS10       -172.386       -77.0717       18.5       19.0       19         WRS11       -172.788       -77.0755       16.5       17.0       19         WRS12       -173.203       -77.0892       14.5       15.0       19         WRS14       -174.005       -77.1055       13.5       14.0       19         WRS17       -175.215       -77.1052       20.4       21.0       19         WRS21       -176.826       -77.1051       23.4       24.0       19         WRS2       -169.226       -77.1021       23.3       24.0       19         WRS2       -169.618       -77.1018       16.5       17.0       19         WRS3       -169.618       -77.1018       16.5       17.0       19	WHIT	-104.3867	-82.6823	31.5	30.2	<u>9</u>
WM72         11.524         -72.144         50.0         47.4         6           WM73         11.562         -71.437         45.0         43.6         6           WM79         13.215         -72.04         51.0         48.6         9           WNDY         -119.4129         -82.3695         23.17         22.2         9           WRS10         -172.386         -77.0717         18.5         19.0         19           WRS11         -172.788         -77.0755         16.5         17.0         19           WRS12         -173.203         -77.0892         14.5         15.0         19           WRS14         -174.005         -77.1055         13.5         14.0         19           WRS17         -175.215         -77.1052         20.4         21.0         19           WRS21         -176.826         -77.1051         23.4         24.0         19           WRS2         -169.226         -77.0939         15.5         16.0         19           WRS25         -178.445         -77.1214         23.3         24.0         19           WRS3         -169.618         -77.1021         16.5         17.0         19	WILS	-80.5587	-80.0396	30	29.3	<u>9</u>
WM73         11.562         -71.437         45.0         43.6         6           WM79         13.215         -72.04         51.0         48.6         6           WNDY         -119.4129         -82.3695         23.17         22.2         9           WRS10         -172.386         -77.0717         18.5         19.0         19           WRS11         -172.788         -77.0755         16.5         17.0         19           WRS12         -173.203         -77.0892         14.5         15.0         19           WRS14         -174.005         -77.1055         13.5         14.0         19           WRS14         -174.005         -77.1052         20.4         21.0         19           WRS17         -175.215         -77.1051         23.4         24.0         19           WRS21         -176.826         -77.1051         23.4         24.0         19           WRS2         -169.226         -77.1039         15.5         16.0         19           WRS2         -179.937         -77.1218         23.3         24.0         19           WRS3         -169.618         -77.1018         16.5         17.0         19	WM72	11.524	-72.144	50.0	47.4	<u>6</u>
WM79         13.215         -72.04         51.0         48.6         9           WNDY         -119.4129         -82.3695         23.17         22.2         2           WRS10         -172.386         -77.0717         18.5         19.0         19           WRS11         -172.788         -77.0755         16.5         17.0         12           WRS11         -172.788         -77.0755         16.5         17.0         19           WRS12         -173.203         -77.0892         14.5         15.0         19           WRS14         -174.005         -77.1055         13.5         14.0         19           WRS14         -174.005         -77.1052         20.4         21.0         19           WRS11         -176.826         -77.1051         23.4         24.0         19           WRS2         -169.226         -77.0939         15.5         16.0         19           WRS25         -178.445         -77.1214         23.3         24.0         19           WRS3         -169.618         -77.1018         16.5         17.0         19           WRS4         -169.986         -77.0716         18.5         19.0         19	WM73	11.562	-71.437	45.0	43.6	<u>6</u>
WNDY       -119.4129       -82.3695       23.17       22.2       9         WRS10       -172.386       -77.0717       18.5       19.0       19         WRS11       -172.788       -77.0755       16.5       17.0       19         WRS12       -173.203       -77.0892       14.5       15.0       19         WRS14       -174.005       -77.1055       13.5       14.0       19         WRS14       -174.005       -77.1052       20.4       21.0       19         WRS17       -175.215       -77.1051       23.4       24.0       19         WRS21       -176.826       -77.1051       23.4       24.0       19         WRS2       -169.226       -77.1039       15.5       16.0       19         WRS2       -169.226       -77.1214       23.4       24.0       19         WRS25       -178.445       -77.1218       23.3       24.0       19         WRS3       -169.618       -77.1021       16.5       17.0       19         WRS4       -169.986       -77.1021       16.5       17.0       19         WRS6       -170.773       -77.0539       19.6       20.0       19     <	WM79	13.215	-72.04	51.0	48.6	<u>6</u>
WRS10       -172.386       -77.0717       18.5       19.0       12         WRS11       -172.788       -77.0755       16.5       17.0       12         WRS12       -173.203       -77.0892       14.5       15.0       12         WRS14       -174.005       -77.1055       13.5       14.0       12         WRS14       -174.005       -77.1052       20.4       21.0       12         WRS17       -175.215       -77.1052       20.4       21.0       12         WRS21       -176.826       -77.1051       23.4       24.0       12         WRS2       -169.226       -77.0939       15.5       16.0       12         WRS2       -169.226       -77.1214       23.4       24.0       12         WRS2       -169.226       -77.1214       23.3       24.0       12         WRS3       -169.618       -77.1218       23.3       24.0       12         WRS4       -169.986       -77.1021       16.5       17.0       12         WRS6       -170.773       -77.0716       18.5       19.0       12         WRS7       -171.18       -77.0539       19.6       20.0       12 <td>WNDY</td> <td>-119.4129</td> <td>-82.3695</td> <td>23.17</td> <td>22.2</td> <td>2</td>	WNDY	-119.4129	-82.3695	23.17	22.2	2
WRS11       -172.788       -77.0755       16.5       17.0       19         WRS12       -173.203       -77.0892       14.5       15.0       19         WRS14       -174.005       -77.1055       13.5       14.0       19         WRS17       -175.215       -77.1052       20.4       21.0       19         WRS21       -176.826       -77.1051       23.4       24.0       19         WRS2       -169.226       -77.0939       15.5       16.0       19         WRS2       -169.226       -77.1214       23.4       24.0       19         WRS2       -169.226       -77.1214       23.4       24.0       19         WRS2       -169.237       -77.1218       23.3       24.0       19         WRS3       -169.618       -77.1018       16.5       17.0       19         WRS4       -169.986       -77.1021       16.5       17.0       19         WRS6       -170.773       -77.0716       18.5       19.0       19         WRS7       -171.18       -77.0539       19.6       20.0       19         WRS8       -171.58       -77.0551       20.5       21.0       19	WRS10	-172.386	-77.0717	18.5	19.0	<u>19</u>
WRS12       -173.203       -77.0892       14.5       15.0       19         WRS14       -174.005       -77.1055       13.5       14.0       19         WRS17       -175.215       -77.1052       20.4       21.0       19         WRS21       -176.826       -77.1051       23.4       24.0       19         WRS2       -169.226       -77.0939       15.5       16.0       19         WRS25       -178.445       -77.1214       23.4       24.0       19         WRS29       -179.937       -77.1218       23.3       24.0       19         WRS3       -169.618       -77.1018       16.5       17.0       19         WRS4       -169.986       -77.1021       16.5       17.0       19         WRS6       -170.773       -77.0716       18.5       19.0       19         WRS7       -171.18       -77.0539       19.6       20.0       19         WRS8       -171.58       -77.0551       20.5       21.0       19         WRS9       -171.988       -77.0641       20.5       21.0       19         WRS9       -171.988       -77.0641       20.5       21.0       19	WRS11	-172.788	-77.0755	16.5	17.0	<u>19</u>
WRS14       -174.005       -77.1055       13.5       14.0       19         WRS17       -175.215       -77.1052       20.4       21.0       19         WRS21       -176.826       -77.1051       23.4       24.0       19         WRS2       -169.226       -77.0939       15.5       16.0       19         WRS2       -169.226       -77.1214       23.4       24.0       19         WRS25       -178.445       -77.1214       23.4       24.0       19         WRS29       -179.937       -77.1218       23.3       24.0       19         WRS3       -169.618       -77.1018       16.5       17.0       19         WRS4       -169.986       -77.1021       16.5       17.0       19         WRS6       -170.773       -77.0716       18.5       19.0       19         WRS7       -171.18       -77.0539       19.6       20.0       19         WRS8       -171.58       -77.0551       20.5       21.0       19         WRS9       -171.988       -77.0641       20.5       21.0       19         ZHSH       76.3727       -69.3747       38.3       38.3       13	WRS12	-173.203	-77.0892	14.5	15.0	<u>19</u>
WRS17       -175.215       -77.1052       20.4       21.0       19         WRS21       -176.826       -77.1051       23.4       24.0       19         WRS2       -169.226       -77.0939       15.5       16.0       19         WRS25       -178.445       -77.1214       23.4       24.0       19         WRS29       -179.937       -77.1214       23.3       24.0       19         WRS3       -169.618       -77.1018       16.5       17.0       19         WRS4       -169.986       -77.1021       16.5       17.0       19         WRS6       -170.773       -77.0716       18.5       19.0       19         WRS7       -171.18       -77.0539       19.6       20.0       19         WRS8       -171.58       -77.0551       20.5       21.0       19         WRS9       -171.988       -77.0641       20.5       21.0       19         WRS9       -171.988       -77.0641       20.5       21.0       19         ZHSH       76.3727       -69.3747       38.3       38.3       13	WRS14	-174.005	-77.1055	13.5	14.0	<u>19</u>
WRS21       -176.826       -77.1051       23.4       24.0       19         WRS2       -169.226       -77.0939       15.5       16.0       19         WRS25       -178.445       -77.1214       23.4       24.0       19         WRS29       -179.937       -77.1218       23.3       24.0       19         WRS3       -169.618       -77.1018       16.5       17.0       19         WRS4       -169.986       -77.1021       16.5       17.0       19         WRS6       -170.773       -77.0716       18.5       19.0       19         WRS7       -171.18       -77.0539       19.6       20.0       19         WRS8       -171.58       -77.0551       20.5       21.0       19         WRS9       -171.988       -77.0641       20.5       21.0       19         ZHSH       76.3727       -69.3747       38.3       38.3       13	WRS17	-175.215	-77.1052	20.4	21.0	<u>19</u>
WRS2       -169.226       -77.0939       15.5       16.0       19         WRS25       -178.445       -77.1214       23.4       24.0       19         WRS29       -179.937       -77.1218       23.3       24.0       19         WRS3       -169.618       -77.1018       16.5       17.0       19         WRS4       -169.986       -77.1021       16.5       17.0       19         WRS6       -170.773       -77.0716       18.5       19.0       19         WRS7       -171.18       -77.0539       19.6       20.0       19         WRS8       -171.58       -77.0551       20.5       21.0       19         WRS9       -171.988       -77.0641       20.5       21.0       19         ZHSH       76.3727       -69.3747       38.3       38.3       13	WRS21	-176.826	-77.1051	23.4	24.0	<u>19</u>
WRS25       -178.445       -77.1214       23.4       24.0       19         WRS29       -179.937       -77.1218       23.3       24.0       19         WRS3       -169.618       -77.1018       16.5       17.0       19         WRS4       -169.986       -77.1021       16.5       17.0       19         WRS6       -170.773       -77.0716       18.5       19.0       19         WRS7       -171.18       -77.0539       19.6       20.0       19         WRS8       -171.58       -77.0641       20.5       21.0       19         WRS9       -171.988       -77.0641       20.5       21.0       19         ZHSH       76.3727       -69.3747       38.3       38.3       13	WRS2	-169.226	-77.0939	15.5	16.0	<u>19</u>
WRS29       -179.937       -77.1218       23.3       24.0       19         WRS3       -169.618       -77.1018       16.5       17.0       19         WRS4       -169.986       -77.1021       16.5       17.0       19         WRS6       -170.773       -77.0716       18.5       19.0       19         WRS7       -171.18       -77.0539       19.6       20.0       19         WRS8       -171.58       -77.0551       20.5       21.0       19         WRS9       -171.988       -77.0641       20.5       21.0       19         ZHSH       76.3727       -69.3747       38.3       38.3       13	WRS25	-178.445	-77.1214	23.4	24.0	<u>19</u>
WRS3       -169.618       -77.1018       16.5       17.0       19         WRS4       -169.986       -77.1021       16.5       17.0       19         WRS6       -170.773       -77.0716       18.5       19.0       19         WRS7       -171.18       -77.0539       19.6       20.0       19         WRS8       -171.58       -77.0551       20.5       21.0       19         WRS9       -171.988       -77.0641       20.5       21.0       19         ZHSH       76.3727       -69.3747       38.3       38.3       13	WRS29	-179.937	-77.1218	23.3	24.0	<u>19</u>
WRS4       -169.986       -77.1021       16.5       17.0       19         WRS6       -170.773       -77.0716       18.5       19.0       19         WRS7       -171.18       -77.0539       19.6       20.0       19         WRS8       -171.58       -77.0551       20.5       21.0       19         WRS9       -171.988       -77.0641       20.5       21.0       19         ZHSH       76.3727       -69.3747       38.3       38.3       13	WRS3	-169.618	-77.1018	16.5	17.0	<u>19</u>
WRS6         -170.773         -77.0716         18.5         19.0         19           WRS7         -171.18         -77.0539         19.6         20.0         19           WRS8         -171.58         -77.0551         20.5         21.0         19           WRS9         -171.988         -77.0641         20.5         21.0         19           ZHSH         76.3727         -69.3747         38.3         38.3         13	WRS4	-169.986	-77.1021	16.5	17.0	<u>19</u>
WRS7         -171.18         -77.0539         19.6         20.0         19           WRS8         -171.58         -77.0551         20.5         21.0         19           WRS9         -171.988         -77.0641         20.5         21.0         19           ZHSH         76.3727         -69.3747         38.3         38.3         13	WRS6	-170.773	-77.0716	18.5	19.0	<u>19</u>
WRS8         -171.58         -77.0551         20.5         21.0         19           WRS9         -171.988         -77.0641         20.5         21.0         19           ZHSH         76.3727         -69.3747         38.3         38.3         13	WRS7	-171.18	-77.0539	19.6	20.0	<u>19</u>
WRS9         -171.988         -77.0641         20.5         21.0         19           ZHSH         76.3727         -69.3747         38.3         38.3         13	WRS8	-171.58	-77.0551	20.5	21.0	<u>19</u>
ZHSH 76.3727 -69.3747 38.3 38.3 <sup>13</sup>	WRS9	-171.988	-77.0641	20.5	21.0	<u>19</u>
	ZHSH	76.3727	-69.3747	38.3	38.3	<u>13</u>

2060 Note: data sources are:

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Figure S2









-1.0 -0.5 0.0 0.5 1.0 S-wave velocity anomaly (%)



Figure S5





